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## Dual 16 Bit, 1.25GSPS Signal Processing DAC with JESD204A Serial Interface

Preliminary Technical Data **AD9128** 

### **FEATURES**

**Low power: 1.4 W @ 1.0 GSPS, 1.2 @ 614 MSPS, full operating conditions Data Interface through Four 3.125Gbps JESD204A compliant data lanes Single carrier WCDMA ACLR = 76 dBc @ 80 MHz IF Analog output: adjustable 8.7 mA to 31.7 mA, RL = 25 Ω to 50 Ω 2x/4x/8x interpolator/complex modulator allows carrier placement anywhere in DAC bandwidth Multi-chip synchronization interface with latency locking High performance, low noise PLL clock multiplier Digital inverse sinc filter 56-lead, exposed paddle LFCSP package** 

### **APPLICATIONS**

**Wireless infrastructure Transmit diversity Wideband communications: LMDS/MMDS, point-to-point** 

#### **GENERAL DESCRIPTION**

The AD9128 is a dual, 16-bit, high dynamic range, digital-toanalog converter (DAC) that provides a sample rate of 1.25 GSPS, permitting a multi-carrier generation up to the Nyquist frequency. The AD9128 includes features optimized for direct conversion transmit applications, including complex digital modulation, and gain and offset compensation. The DAC outputs can interface seamlessly with Analog Devices'

quadrature modulators such as the ADL537x Broadband QMOD series.

The AD9128 incorporates four high-speed serial data lanes reducing the interface connections between the DAC and its digital companion chip compared with CMOS or LVDS parallel interfaces. The serial interfaces are capable of receiving data with voltage swings of 200 to  $700 \text{mV}_{p-p}$ . With 3 dB of typical receiver equalization, the receiver is capable of capturing data sent across 0 to 20 cm traces on an FR4 board. The AD9128 also features multi-chip deterministic latency capability, allowing multiple dual DACs to be in alignment with one another.

A serial port interface provides read/write access to on-chip registers. Full-scale output current is programmable over a range of 8.5 mA to 31 mA. TheAD9128 operates on 1.8 V and 3.3 V supply rails.

#### **PRODUCT HIGHLIGHTS**

- 1. Small package size 8mm x 8mm footprint
- 2. Fewer pins for data input word width with only Four JESD204A data lines
- 3. Ultra low noise and intermodulation distortion (IMD) enables high quality transmission of wideband signals from baseband to high intermediate frequencies.
- 4. A proprietary DAC output switching technique enhances dynamic performance.



Figure 1. Typical signal chain with simplified block diagram of the AD9128

#### **Rev. PrI**

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### FUNCTIONAL BLOCK DIAGRAM



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### **SPECIFICATIONS**

### **DC SPECIFICATIONS**

 $T<sub>MIN</sub>$  to  $T<sub>MAX</sub>$ , AVDD33 = 3.3 V, IOVDD = 3.3V, DVDD18 = SVDD = PLLVDD = VTTVDD = CVDD18 =1.8 V, I<sub>OUTFS</sub> = 20 mA, maximum sample rate, unless otherwise noted.

#### **Table 1. DC Specifications**



#### **DIGITAL SPECIFICATIONS**

 $T_{MIN}$  to  $T_{MAX}$ , AVDD33 = 3.3 V, IOVDD = 3.3V, DVDD18 = SVDD = PLLVDD = VTTVDD = CVDD18 =1.8 V, I<sub>OUTFS</sub> = 20 mA, maximum sample rate, unless otherwise noted.

#### **Table 2. Digital specifications**





### **DIGITAL INPUT DATA TIMING**

#### **Table 3. Input data timing specifications**



#### **AC SPECIFICATIONS**

TMIN to TMAX, AVDD33 = 3.3 V, IOVDD = 3.3V, DVDD18 = SVDD = PLLVDD = VTTVDD = CVDD18 =1.8 V, IOUTFs = 20 mA, maximum sample rate, unless otherwise noted.

#### **Table 4. AC Specifications**



### ABSOLUTE MAXIMUM RATINGS





Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

#### **THERMAL RESISTANCE**

 $\theta_{\rm JA}$  is specified for the worst-case conditions, that is, a device soldered in a circuit board for surface-mount packages.

#### **Table 6. Thermal Resistance**



#### **ESD CAUTION**



ESD (electrostatic discharge) sensitive device. Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

### PIN CONFIGURATION AND FUNCTION DESCRIPTIONS



Figure 2.

#### **Table 7. Pin List and Description**



<sup>1</sup> Single Edge DAC Alignment input if PLL is disabled. LVDS resistor required between this pin and REFCLK in align mode.





### TYPICAL PERFORMANCE CHARACTERISTICS



Figure 5

### **TERMINOLOGY**

#### **Integral Nonlinearity (INL)**

INL is the maximum deviation of the actual analog output from the ideal output, determined by a straight line drawn from zero scale to full scale.

#### **Differential Nonlinearity (DNL)**

DNL is the measure of the variation in analog value, normalized to full scale, associated with a 1 LSB change in digital input code.

#### **Offset Error**

Offset error is the deviation of the output current from the ideal of 0 mA. For IOUT1P, 0 mA output is expected when all inputs are set to 0. For IOUT1N, 0 mA output is expected when all inputs are set to 1.

#### **Gain Error**

Gain error is the difference between the actual and ideal output span. The actual span is determined by the difference between the output when all inputs are set to 1 and the output when all inputs are set to 0.

#### **Output Compliance Range**

The output compliance range is the range of allowable voltage at the output of a current output DAC. Operation beyond the maximum compliance limits can cause either output stage saturation or breakdown, resulting in nonlinear performance.

#### **Temperature Drift**

Temperature drift is specified as the maximum change from the ambient (25°C) value to the value at either  $T<sub>MIN</sub>$  or  $T<sub>MAX</sub>$ . For offset and gain drift, the drift is reported in ppm of fullscale range (FSR) per degree Celsius. For reference drift, the drift is reported in ppm per degree Celsius.

#### **Power Supply Rejection (PSR)**

PSR is the maximum change in the full-scale output as the supplies are varied from minimum to maximum specified voltages.

#### **Settling Time**

Settling time is the time required for the output to reach and remain within a specified error band around its final value, measured from the start of the output transition.

#### **Spurious Free Dynamic Range (SFDR)**

SFDR is the difference, in decibels, between the peak amplitude of the output signal and the peak spurious signal within the dc to Nyquist frequency of the DAC. Typically, energy in this band is rejected by the interpolation filters. This specification, therefore, defines how well the interpolation filters work and the effect of other parasitic coupling paths on the DAC output.

#### **Signal-to-Noise Ratio (SNR)**

SNR is the ratio of the rms value of the measured output signal to the rms sum of all other spectral components below the Nyquist frequency, excluding the first six harmonics and dc. The value for SNR is expressed in decibels.

#### **Interpolation Filter**

If the digital inputs to the DAC are sampled at a multiple rate of fDATA (interpolation rate), a digital filter can be constructed that has a sharp transition band near fDATA/2. Images that typically appear around f<sub>DAC</sub> (output data rate) can be greatly suppressed.

#### **Adjacent Channel Leakage Ratio (ACLR)**

ACLR is the ratio in decibels relative to the carrier (dBc) between the measured power within a channel relative to its adjacent channel.

#### **Complex Image Rejection**

In a traditional two-part upconversion, two images are created around the second IF frequency. These images have the effect of wasting transmitter power and system bandwidth. By placing the real part of a second complex modulator in series with the first complex modulator, either the upper or lower frequency image near the second IF can be rejected.

#### **Current Mode Logic (CML)**

CML is a differential digital logic family. Signal transmission is point-to-point, unidirectional and terminated at the destination with 50  $\Omega$  resistors to a voltage, VTT, on both differential lines. CML is the physical layer for JESD204.

### THEORY OF OPERATION

The AD9128 is a 16-bit Dual DAC with a SERDES interface that is fully compliant with the JESD204A specifications. Figure *8* shows a top-level diagram of the AD9128. Four high-speed serial lanes carry data with a maximum speed of 3.125Gbps, resulting in a 312.5 MSPS (maximum) input data rate for each of the two DACs. The AD9128 can be configured to operate in 1, 2 or 4 JESD204A lane modes, depending on the required DAC input data rate. It can also operate in single DAC mode, with either 1-lane or 2-lane mode.

The two DACs can operate as I and Q channels in a direct conversion transmitter. Or as two independent DACs running at the same DAC sampling rate. The digital data-path of the AD9128 offers four interpolation modes (1X, 2X, 4X or 8X) through three half-band filters with a maximum DAC sampling rate of 1.25 GSPS.

FDAC is the DAC sampling frequency. The input signal data-rate for both DACs is  $F_{DAC} \div$  the interpolation factor.

For I/Q applications a Numerically Controlled Oscillator (NCO) provides a means for modulating the signal with a programmable carrier signal. The NCO generates the carrier signal for a complex modulator in the digital data path. The resolution of the NCO is 32 bits, allowing the signal to be placed in the output spectrum with very fine resolution. The **AD9128 Startup** Sequence). The following sections describe elements of the AD9128 in detail.

AD9128 also features coarse modulation. Coarse modulation up converts a digital signal centered at DC center frequency of F<sub>DAC</sub>/4. This option consumes significantly less power compared with the NCO modulation approach. Digital gain, offset and phase compensation are included in the AD9128 to help with unwanted sideband suppression in direct conversion transmitters. An inverse Sinc filter is provided to compensate for DAC output sinc-related roll-off.

The DAC Clock (DACCLK) can be sourced externally. Or generated on chip using a PLL synthesizer with externally supplied reference signal.

The AD9128 DAC core provides a fully differential current output with a nominal full-scale current of 20mA. The full-scale current is user adjustable between 8.7mA and 31.7mA. The differential current outputs are complementary.

The AD9128 is capable of multi-chip synchronization and can both synchronize devices and establish deterministic latency (latency locking) among multiple AD9128 devices. The latency for each of the DACs remains constant from link establishment to link establishment.

A SPI interface provides read and write access to registers. The various functional blocks and the data interface need to be setup in a specific sequence for proper operation (See section



Figure 8. AD9128 Functional Block Diagram

### HIGH SPEED SERIAL DATA INTERFACE

The AD9128 has four JESD204A data ports that receive data for both I and Q transmit paths. Figure *9* describes the communication layers implemented in the AD9128 for each high speed serial data interface to recover the clock, descramble and deserialize the data before it is sent to the Digital Signal Processing section of the AD9128. If a lower data speed is

acceptable the part can be configured to operate with either two or one JESD204A lanes. The maximum data speed is directly linked to the number of lanes used. In the 4 lane, 2 lane and 1 lane configurations, the maximum supported data speeds are 312.5 MSPS, 156.25 MSPS and 78.125 MSPS respectively.



*Figure 9. Functional block diagram of Serial receiver* 

As the AD9128 can operate with more than one active high speed serial data lane, both achieving synchronization and handling loss of synchronization of the lanes are very important. To simplify the interface to the companion digital chip, theAD9128 designates one master signal (SYNCb) as far as multiple lane synchronization is concerned. If one lane loses synchronization, a resynchronization request is sent to the transmitter and the transmitter stops sending data to all lanes until resynchronization has been achieved.

#### **RECEIVER CIRCUIT**

The AD9128 provides four 1.8V differential serial input interfaces compliant with the JESD204A specifications. These interfaces can accept signals at frequencies up to 3.125Gbps using the input topology in Figure *10*.



*Figure 10. Receiver line termination*

The receiver eye mask in Figure 11 specifies the signal amplitude and jitter tolerance for the AD9128 High Speed Serial Data Interface receiver.



*Figure* 11*. Receiver Eye Mask* 

The receiver is equipped with a Clock/Data Recovery circuit (CDR) based on a PLL. The PLL effectively multiplies the Frame clock input by 5 X F (F=Number of bytes per frame) and the CDR synchronizes the phase used to sample the data on each serial lane independently. This independent phase adjustment per serial interface ensures accurate data sampling and eases the implementation of multiple serial interfaces on a PCB. A byte rate PLL clock is then used in the link layer, descrambler and transport layers to deserialize the serial input and provide data to the DAC inputs.

### **LINK LAYER**

The AD9128 can operate with more than one active high speed serial data interface. Link layer communications such as code group synchronization, frame alignment and frame synchronization are handled by all four lanes. However, the configuration data is always checked only on a single logical high speed serial data interface: LN0. This logical serial interface can be connected to any of the four JESD204A physical receivers RXn. It is important to note that logical LN0 must be active in all modes of operation.

The AD9128 decodes 8B/10B control characters allowing marking of start and end of frame and alignment between serial lanes. The AD9128 serial interface can issue a synchronization

request by setting the SYNCb pin low. The synchronization protocol follows the JESD204A standard. When a stream of 8 consecutive /K/ symbols is received, the AD9128 deactivates the synchronization request by setting SYNCb pin high and waits for the transmitter to issue an Initial Lane Alignment Sequence (ILAS).

#### **DESCRAMBLER**

The AD9128 provides an optional descrambler block using a self-synchronous descrambler with polynomial:  $1 + x^{14} + x^{15}$ .

Data scrambling can be selected at the transmitter to reduce spectral peaks that would be produced when the same data octets repeat from frame to frame. Another advantage of scrambling is that it makes the spectrum data independent so that possible frequency-selective effects on the electrical interface will not cause data-dependent errors.

#### **TRANSPORT LAYER**

The transport layer maps the incoming descrambled data to DAC samples. It provides control of the JESD204A parameters shown in Table 8.

#### **Table 8. JESD204A Transport Layer Parameters**



Since the AD9128 uses the Frame input as the reference clock for the deserializer PLL, the Frame input needs to be greater than 50 MHz. A number of transport layer configurations are defined to fit the AD9128 definition, as shown in

Table **9**.

#### **Table 9. JESD204A Configuration Parameters**



Since the AD9128 has four high speed serial data interfaces, several combinations of lanes per converter can be used depending on the data rate desired.

The AD9128 can also operate in real single-DAC mode. In this case, it can be configured in either 2-lane or 1-lane mode (Note: all 4 lanes cannot be used in single-DAC mode). The maximum input data rate in single-DAC mode is the same as the dual DAC mode (312.5MHz).

#### **Table 10. AD9128 interface speeds**











Figure 14. Serial data interface with 1 lane active

#### **JESD204A SERIAL LINK ESTABLISHMENT**

A brief summary of the high speed serial link establishment process is given below. Please see the JESD204A Specifications document (reference) for complete details.

- 1. Code group synchronization
	- a. Each receiver must locate K (K28.5) characters in its input data stream
- b. Once 8 consecutive K characters have been detected on all link lanes, the receiver block de-asserts the SYNCb signal to the transmitter block.
- c. The transmitter captures the change in SYNCb and after a fixed number of frame clocks, starts the Initial Lane Alignment Sequence (ILAS).
- 2. Initial Lane Alignment Sequence
	- The main purposes of this phase are to align all the lanes of the link and verify the parameters of the link.
	- b. Before the link is established, each of the link parameters is written to the receiver device to designate how data will be sent to the receiver block.
	- c. ILAS consists of 4 or more multi-frames. The last character or each multi-frame is a multi-frame alignment character /A/
	- d. The first, third, and fourth multi-frames are populated with pre-determined data values. The de-framer uses the final /A/ of each lane to align the ends of the multi-frames within the receiver.
	- e. The second multi-frame contains an R (K.28.0), Q(K.28.4), and then data corresponding to the link parameters.
	- f. Additional multi-frames can be added to ILAS if needed by the receiver. The AD9128 uses 8 multiframes in its ILAS. (When alignment scheme or deterministic latency are used.)
	- g. After the last /A/ character of the last ILAS multiframe data begins to be streamed.
- 3. Data Streaming
	- a. In this phase data is streamed from the transmitter block to the receiver block.
	- b. Data can be optionally scrambled. Scrambling does not start until the very first octet following the ILAS.
	- c. The receiver block processes and monitors the data it receives for errors including:
		- i. Bad running disparity (8b/10b error)
		- ii. Not in Table (8b/10b error)
		- iii. Unexpected control-character
		- iv. Bad ILAS
		- v. Inter-lane skew error (through character replacement)
	- d. If any of these errors exists, it is reported back to the transmitter in one of a few ways
		- i. SYNCb assertion: Resynchronization (SYNCb pulled low) is called for at each error. For the first

three errors, SYNCb is asserted after an error counter reaches a given error threshold.

- ii. SYNCb reporting: SYNCb is pulsed low for a frame clock period if an error occurs
- iii. Reporting may also be done via interrupt (not covered by the JESD204A specification). See (i) for error thresholds.

### **FIFO OPERATION**

The AD9128 contains several stages of FIFO to deal with the high speed serial data interface protocol and to synchronize the data input with the DAC clock input (See Figure 15).

The FIFO in the SERDES deframer interface is used to synchronize the samples sent on the high speed serial data interface with the deframer clock. This FIFO absorbs timing variations between the data source and the deframer. When the FIFO reaches either full or empty state, it is recommended that the user reset it through Register 35 bit 0 and, if necessary, reestablish the SERDES data link. Note that resetting the SERDES link does not reset the FIFO to half-full automatically.

A second 2 channel x 16-bit wide, 8- word deep FIFO exists in the DAC (datapath FIFO) to absorb timing variations between the DAC clock and the Deframer clock. Figure 16 shows the block diagram of the data path through the FIFO. The data is latched into the device, formatted and then written into the FIFO register determined by the FIFO write-pointer. The value of the write-pointer is incremented every time a new word is loaded into the FIFO. Meanwhile, data is read from the FIFO register determined by the read-pointer and fed into the digital datapath. The value of the read-pointer is updated every rising edge of the internal DAC based data clock. The one exception to this occurs when a resynchronization request is in progress: the write side of the FIFO does not increment and the read side is held in reset at a fixed value. Once the ILAS is completed in the AD9128, then the Datapath FIFO is automatically reset to "half full". During a synchronization request, the DAC outputs are forced to mid-scale and the datapath is flushed. This is done to prevent corrupted data from passing from the DAC.

Valid data will be transmitted through the FIFOs as long as the FIFOs do not overflow or become empty. Nominally, data will be written to the FIFO at the same rate as data is read from the FIFO. This keeps the data level in the FIFO constant. If data is written to the FIFO faster than data is read, the data level in the FIFO increases. If the data is written to the device slower than data is read, the data level in the FIFO decreases.



*Figure 16 – Block Diagram of Datapath FIFO* 

### **FRAME CLOCKING**

The frame clock is the master reference for the high speed serial interface of the AD9128. It drives a PLL in the JESD204A part of the system and needs to be set to the input data rate of the system. The user has three options for the frame clock in AD9128:

- Externally sourced through pins JESD\_FRAMEP/N: the input should be AC coupled and will be self-biased internally.
- Externally sourced through REFCLKP/N: this is possible only if the internal DAC PLL is used and the supplied reference clock supplied to the PLL (via REFCLKP/N) is at the data rate of the system. (abd equal to the FRAME rate) The input should be AC coupled and will be self-biased internally.
- Internally sourced by using a divided down version of the DAC clock: this helps minimize the number of low frequency clocks in the user system.

The frame clock source is controlled and monitored through register 0x001D.

### **SERDES PLL**

The SERDES PLL generates clocks at half the rate of the serial data rate and supplies them to the Clock and Data Recovery

(CDR) block. The SERDES PLL settings are controlled and monitored in the register 0x01E. The PLL divide ratio (register 0x01E, bits [3:0]) is dependent on the F value (number of bytes per frame) of the JESD204A link. The F value of the link (1,2 or 4) should be written to this register. The SERDES PLL can be monitored for lock by reading register 0x01E, bit 6.

The SERDES PLL lock can also be accessed through the interrupt controller by writing Register 0x006, bits 7 and/or 6 high. Bit7 enables the interrupt if the SERDES PLL has lost lock, and Bit6 enables the interrupt if the SERDES PLL is locked. These interrupts can be found by reading register 0x009 bits 7 and 6 (when the interrupt output of the AD9128 falls,).

Note that the SERDES PLL must lock before parameters can be written to the deframer.

### **CONFIGURING THE JESD204A SERIAL INTERFACE**

After the SERDES PLL has been successfully locked, the Deserializer SPI is available and can be verified by reading register 0x02 bit 0. The Deserializer SPI is a synchronous read/write SPI (See section *Serial Peripheral Interface* for SPI interface details). It is addressed through the long addressing mode (default for the AD9128). The addresses for this part of the circuit range from 0x100-0x17F.

#### **Input termination**

The AD9128 will auto-calibrate to 50 ohms termination on power-up as register 0x010 bit 5 has a default setting of high. The auto-calibrated value found will be held constant until bit 5 is disabled. Alternatively, a manual calibration value can be entered through register 0x011 bit 3:0 (highest resistor value is 0000 and lowest value is 1111). Manual calibration requires register 0x10 bit5 to be low and 0x11 bit4 to be high. All settings for input termination can be setup and controlled through registers 0x010 and 0x011.

The input termination voltage of the DAC can be sourced either externally or internally:

- External: An external voltage can be driven through the VTT pin. In order to support DC compliance, its value should match the common mode voltage of the CML driver at the transmitter. It may be bypassed at the pin to local ground.
- Internal: The termination voltage can be supplied internally by enabling register 0x010 bit 4. The VTT buffer drives both the internal VTT termination and the VTT pin. The termination voltage value can be set through register 0x010 its 3:0. In this case, the VTT pin should not be bypassed to ground. As in option 1, to meet DC compliance, the value of the voltage should be chosen to be close to the value of the CML driver output common-mode. This will ensure minimum power consumption.

For AC coupled systems, in order to minimize power consumption, VTT should be set close to 600mV.

#### **Clock Data Recovery (CDR)**

The CDR circuits for the four lanes of the high speed serial interface can be enabled through register 0x012 bits 3:0. For two-lane or one-lane operation, any of the two or any one lane can be chosen. Unused lanes, if enabled, will consume unnecessary power.

#### **Logical Lane Mapping/Enabling**

Each of the four physical high speed serial interface lanes, if used, must be mapped to an appropriate logical lane. For example, if four physical lanes are enabled for use with two converters then each of the four logical lanes are mapped to a distinct physical lane. Logical lanes 0, 1, 2 and 3 will contain IMSB, ILSB, QMSB, QLSB respectively. The logical lanes are enabled through register 0x17D and their mapping is controlled through register 0x016, as shown in **Table 11**.

#### **Table 11. Logical lane mapping for JESD204A link**



Each of the input lanes can be individually controlled as far as serial symbol mapping is concerned. Both the ordering of the bits (MSB to LSB or LSB to MSB) on bits 7:4, and the individual polarities on bits 3:0 are controlled through register 0x017.

A few mode bits are required in order to operate the non default mode of 4 Lanes or 2 Lanes and  $F = 1$ . These are contained in the Register 0x177. They enable sub-modes of the base configuration of the deframer:

- If F=2, Register 0x177 bits 5:2 must be set to 0111 (1 lane per DAC) and 0x176 must be set to 2.
- If F=4, Register 0x177 bits 5:2 must be set to 1011 (2 DACs 1 line) and 0x176 must be set to 4.
- If F=1, Register 0x177 bits 5:2 must be set to 0000

#### **Programming the JESD204A link parameters**

This section provides details of the link parameters with respect to the modes of operations supported by the AD9128. The link parameters are programmed through registers 0x150 to 0x15D. In order to achieve an accurate comparison, all the register values must be programmed the same at the transmitter and receiver end of the link.

- 1. 0x150: Provides the DID (Device ID or link ID). This is a comparison only value to identify the link name.
- 2. 0x151 bits 3:0: Provides the BID (Bank ID). It is an extension of the DID and meets the same requirements as the DID.
- 3. 0x152 bits 3:0: Provides the LID0 (lane ID for lane 0 within a link). The AD9128 will check the lane identification values on lane 0 only.
- 4. 0x153 bit7: Enables the scrambling function on the link.
- 5. 0x153 Bits4:0: Provides the number of lanes of the link associated with DID. This value L will be set based on the number of lanes used and is programmed as one less than

the number of lanes. The possible values for different DAC modes are:



6. 0x154: Provides the F value or number of octets per frame per lane. Possible values for different modes are shown in Table 12.

#### **Table 12. JESD204A link "F" value**



- 7. 0x155 bits4:0: Provide the K value (number of frames in a multiframe). This value is programmed at one less than the actual number. For the AD9128, the value can be:
	- $K = 31$  when  $F = 0 0x1F$
	- $K = 31$  or 15 when  $F = 1$  or 3- 0x1F or 0x0
- 8. 0x156: Provides the value of M (number of converters on the DAC used by the link). This value is programmed as one less than the actual number of converters.
	- $\bullet$  2 Converters 0x01
	- 1 Converter 0x00
	- 2 Lanes, 1 DAC  $HD = 1 (0x15A = 0x80$
	- 1 Lane, 1 DAC  $HD = 0$  (0x15A = 0x00)
- 9. 0x157 bits 7:6: Provide number of control words per frame. For the AD9128, this value is always 0 since it does not support control bits.
- 10. 0x157 bits 5:0: Represents the number of bits of resolution of the converter. It is programmed at one less than the actual value. The value is 0x0F for the AD9128.



Figure 21. Interrupt control on the AD9128

- 11. 0x158 bits 5:0: Represents the number of bits in each sample being sent to the deframer. It is programmed at one less than the actual value. The value is 0x0F for the AD9128.
- 12. 0x159: Represents the number of samples per frame per converter and is programmed as one less than actual. The AD9128 supports only  $S = 1$  (Reg. 0x159 set to 0).
- 13. 0x15A bit 7: Represents the high density HD parameter.

14. 0x15A bits 4:0: Represents CF (the number of control words per frame clock per lane). Possible values for register 0x15A are shown in Table 13.

#### **Table 13. JESD204A link "HD" value**



- 15. 0x15B, 0x15C: Reserved fields. Should be set to 0 on both receiver and transmitter ends.
- 16. 0x15D: Checksum value equal to the sum of all the registers from 0x150 to 0x15C modulo 256.

#### **Programming ILAS (Initial Lane Alignment Sequence) length***:*

In the AD9128 the length of the ILAS is programmed in register 0x178. It is programmed as the actual number of multi-frames times four (for a value of 1, the ILAS will be 4 multi-frames long). The AD9128 uses 8 multi-frames during the ILAS to accomplish multichip alignment (or 4 if multi-chip alignment is not needed).

In order to enable multichip alignment or latency locking, register 0x178 should be set to 0x02 and register 0x17B bit 0 should be set to 1. When latency locking/alignment is not needed in the system, register 0x178 should be set to 1 and 0x17B bit 0 to 0.

### **INTERRUPTS AND SYNCB CONTROL**

The deframer monitors the link for errors, and in the AD9128 these errors can be reported back to the transmitter through different methods:

- Through interrupts
- Through the SYNCb signal as frame width assertion pulses on the line
- Through the SYNCb interface as forced SYNC requests.

Figure 27 shows a block diagram of the AD9128 interrupt control. Errors are counted on a lane by lane basis and either an error interrupt or a SYNCb event is triggered as the count reaches an Error Threshold. This threshold is programmed in Register 0x17C. Error counts for each lane can be monitored through the use of Registers 0x16D – 0x16F. The errors that the deframer will detect are: Bad Disparity Error, Not in Table Error, Unexpected control character, Alignment issue, Bad ILS Sequence, Configuration mismatch

The Interrupt request is masked by bits in registers 0x17A and 0x17B as follows:

0x17A, Bit7 – Bad Disparity (set high to trigger Interrupt request) 0x17A, Bit 6 – Not in Table 0x017A, Bit 5 – Unexpected control character 0x017A, Bit 4 – Interlane Alignment good

0x017A, Bit 3 – Good ILAS sequence 0x017A, Bit2 – Good Checksum 0x017A, Bit1 – Good Frame Sync 0x017A, Bit0 – Good Code Group Sync

The SYNCb frame width error reporting can be enabled by setting bit 1 of Register 0x175 high (Bad disparity, not in Table, and Unexpected control character will actuate this error reporting mode).

The SYNC force is masked by bits in 0x17B as follows:

0x17B, Bit7 – Bad disparity error (set high for error to force SYNCb high upon error threshold)

0x17B, Bit6 – Not in Table error

0x17B, Bit5 - Unexpected control character

#### **ENABLING THE LINK**

Once SYNCb setup/calibration is completed and clocks have settled, the link is ready to be established. The link can be established by setting bit 7 of Register 0x00A high. A startup sequence is performed for the delay path from DAC clock to SYNCb.

- 1. The SYNCb phase selector is reset to zero
- 2. The SYNCb FIFO is reset.
- 3. The previously programmed value of the SYNCb launch phase is programmed back to the SYNCb phase selector.

Once the startup sequence concludes inside the DAC, the SYNCb signal is allowed to fall. Conditional upon the link parameters being consistent at both ends and the DAC being able to capture data, the link will be established.

### SERIAL PORT INTERFACE

#### **Serial Port Operation**

The serial port is a flexible, synchronous serial communications port allowing easy interface to many industry-standard microcontrollers and microprocessors. The serial I/O is compatible with most synchronous transfer formats, including both the Motorola SPI® and Intel® SSR protocols. The interface allows read/write access to all registers that configure the AD9128. Single or multiple byte transfers are supported, as well as MSBfirst or LSB-first transfer formats. The serial interface ports can be configured as a single pin I/O (SDIO) or two unidirectional pins for input/output (SDIO/SDO).



There are two phases to a communication cycle with the AD9128. Phase 1 is the instruction cycle (the writing of an instruction byte into the device), coincident with the first eight SCLK rising edges. The instruction byte provides the serial port controller with information regarding the data transfer cycle, Phase 2 of the communication cycle. The Phase 1 instruction byte defines whether the upcoming data transfer is a read or write and the starting register address for the first byte of the data transfer. The first eight SCLK rising edges of each communication cycle are used to write the instruction byte into the device.

A logic high on the  $\overline{\text{CS}}$  pin followed by a logic low resets the serial port timing to the initial state of the instruction cycle. From this state, the next eight rising SCLK edges represent the instruction bits of the current I/O operation.

The remaining SCLK edges are for Phase 2 of the communication cycle. Phase 2 is the actual data transfer between the device and the system controller. Phase 2 of the communication cycle is a transfer of one or more data bytes. Registers change immediately upon writing to the last bit of each transfer byte, except for the frequency tuning word and NCO phase offsets that only change when the frequency update bit (Register 0x026, Bit 0) is set.

#### **Table 14. Serial Port Instruction Byte**



#### **Data Format**

The instruction byte contains the information shown in Table 14. R/W, Bit 7 of the instruction byte determines whether a read or a write data transfer occurs after the instruction byte write. Logic 1 indicates a read operation, and Logic 0 indicates a write operation.

A6 to A0, Bit 6 to Bit 0 of the instruction byte, determine the register that is accessed during the data transfer portion of the communication cycle. For multibyte transfers, A6 is the starting byte address. The remaining register addresses are generated by the device based on the LSB\_FIRST bit (Register 0x000, Bit 6).

#### **SERIAL PORT PIN DESCRIPTIONS**

#### **Serial Clock (SCLK)**

The serial clock pin synchronizes data to and from the device and runs the internal state machines. The maximum frequency of SCLK is 40 MHz. All data input is registered on the rising edge of SCLK. All data is driven out on the falling edge of SCLK.

### **Chip Select (CS)**

An active low input starts and gates a communication cycle. It allows more than one device to be used on the same serial communications lines. The SDO and SDIO pins go to a high impedance state when this input is high. During the communication cycle, chip select should stay low.

#### **Serial Data I/O (SDIO)**

Data is always written into the device on this pin. However, this pin can be used as a bidirectional data line. The configuration of this pin is controlled by Register 0x000, Bit 7. The default is Logic 0, configuring the SDIO pin as unidirectional.

#### **Serial Data Out (SDO)**

Data is read from this pin for protocols that use separate lines for transmitting and receiving data. In the case where the device operates in a single bidirectional I/O mode, this pin does not output data and is set to a high impedance state.

#### **Serial Port Options**

The serial port can support both MSB-first and LSB-first data formats. This functionality is controlled by LSB\_FIRST (Register 0x000, Bit 6). The default is MSB-first (LSB\_FIRST = 0).

When LSB  $FIRST = 0$  (MSB-first), the instruction and data bit must be written from MSB to LSB. Multibyte data transfers in MSB-first format start with an instruction byte that includes the register address of the most significant data byte. Subsequent data bytes should follow from the high address to low address. In MSB-first mode, the serial port internal byte address generator decrements for each data byte of the multibyte communication cycle.

When  $LSB_FIRST = 1$  (LSB-first), the instruction and data bit must be written from LSB to MSB. Multibyte data transfers in LSB-first format start with an instruction byte that includes the register address of the least significant data byte followed by multiple data bytes. The serial port internal byte address generator increments for each byte of the multibyte communication cycle.<br>i INSTRUCTION CYCLE





The serial port controller data address decrements from the data address written toward 0x00 for multibyte I/O operations if the MSB-first mode is active. The serial port controller address increments from the data address written toward 0x7F for multibyte I/O operations if the LSB-first mode is active.





### DIGITAL DATA PATH



Figure 22 –Block Diagram of digital datapath

Figure 22 shows the functionality of the digital datapath. The digital processing includes three half-band interpolation filters, a quadrature modulator with a fine resolution NCO, Phase and Offset adjustment blocks and an inverse sinc filter.

The digital datapath accepts I and Q data streams and processes them as either two real data streams or as a quadrature data stream. To utilize any of the modulation modes, the data must be presented to the device in quadrature. The datapath can be used to process two independent real data streams with any of the interpolation modes. The coarse modulation (Fs/4) block can be used along with any of the interpolation filter modes.

### **INTERPOLATION FILTERS**

The transmit path contains three interpolation filters. Each of the three interpolation filters provides a 2x increase in output data rate. The half-band (HB) filters can be cascaded or bypassed to provide 1x, 2x, 4x or 8x interpolation ratios. The bandwidth of the three half-band filters with respect to the data rate at the filter input is as follows:

- Bandwidth of  $H B1 = 0.8x f_{\text{IN}}$
- Bandwidth of HB2 =  $0.5xf_{N2}$
- Bandwidth of  $HB3 = 0.4x$ f<sub>IN3</sub>

The usable bandwidth is defined as the frequency over which the filters have a passband ripple of less than +/-0.01dB and an image rejection of greater than 85dB.

The fine modulator performs frequency translation by performing a digital quadrature modulation of the input signal with a quadrature LO generated by the on-chip NCO.

- 1. 2x interpolation: Either the first (HB1) or second (HB2) half-band filter can be used for 2x interpolation (Register 0x00F). Figure 18 and Figure 19 show the frequency response when HB1 and HB2 are used respectively. The frequency (x-axis) is normalized to the DAC sample rate. Hence in this case, the bandwidth of HB1 is 0.4\*Fdac or 0.8\*Fdata. Similarly, the bandwidth of HB2 is 0.25\*Fdac or 0.5\*Fdata
- 2. 4x interpolation: It is accomplished using HB1 and HB2 (Register 0x00F). Note that it is not possible to use HB3 when in 4x interpolation mode. Figure 20 shows the frequency response for this case. The usable bandwidth is 0.2\*Fdac or 0.8\*Fdata.

3. 8x interpolation: In this case, all three filters are used. Figure 21 shows the frequency response for 8x interpolation. The usable bandwidth is 0.1\*Fdac or 0.8\*Fdata.







Figure 23. Transfer Function of HB1 in 2x interpolation mode. The frequency axis is normalized to the DAC sample rate.



Figure 24 Transfer Function of HB2 in 2x interpolation mode. The frequency axis is normalized to the DAC sample rate.



Figure 25 Transfer Function of HB1 and HB2 (cascaded) in 4x interpolation mode. The frequency axis is normalized to the DAC sample rate.



Figure 26 Transfer function of cascaded HB1, HB2 and HB3 in 8x interpolation mode



Figure 27 Pass band and stop-band characteristics of HB1. All three filters have pass-band ripple <0.01dB and image rejection > 85 dBc

#### **FINE MODULATION**

The fine modulation makes use of a numerically controlled oscillator, a phase shifter and a complex modulator to provide a means for modulating the signal by a programmable carrier signal. A block diagram of the fine modulator is shown in Figure 28. The fine modulator, in conjunction with the coarse modulator allows the signal to be placed anywhere in the output spectrum with very fine frequency resolution.

The quadrature modulator is used to mix the carrier signal generated by the NCO with the I and Q signals. The NCO produces a quadrature carrier signal to translate a single sideband of the input signal to a new center frequency. A complex carrier signal is a pair of sinusoidal waveforms of the same frequency, offset 90° from each other. The frequency of the complex carrier signal is set via the Frequency Tuning Word [31:0] value in Registers 0x020 thru 0x023.

The NCO operating frequency, f<sub>NCO</sub>, is f<sub>DAC</sub>. The frequency of the complex carrier signal can be set up to  $\frac{1}{2}$  f<sub>NCO</sub> and is calculated as follows:

For 
$$
0 \leq FTW \leq 2^{31}
$$
,  $f_{\text{Carrier}} = \frac{FTW}{2^{32}} \times f_{\text{DAC}}$ 

For 
$$
2^{31} < FTW \leq 2^{32}
$$
,  $f_{Carrier} = \left(1 - \frac{FTW}{2^{32}}\right) \times f_{DAC}$ 

#### **Updating the Frequency Tuning Word**

Unlike the other configuration registers, the frequency tuning word registers do not get updated immediately upon writing. After loading the FTW registers with the desired values, bit 0 of register 0x026 must transition from a 0 to a 1 for the new FTW to take effect.

#### **Phase Offset Adjustment**

A 16-bit phase offset may be added to the output of the phase accumulator via the serial port. This static phase adjustment results in an output signal that is offset by a constant angle relative to the nominal signal. This allows the user to phase align the NCO output with some external signal, if necessary. This can be especially useful when NCOs of multiple AD9128 devices are programmed for synchronization. The phase offset allows for the adjustment of the output timing between the devices. The static phase adjustment is sourced from the NCO Phase Offset Word [15:0] value located in Registers 0x024 and 0x025.



Figure 28 – Fine Modulator Block Diagram

#### **COARSE MODULATION**

The coarse modulation block at the end of the digital datapath provides a digital up-conversion of the incoming data by ¼ of its data rate (which is equal to Fdac, the DAC sampling rate). When a fixed up-conversion of Fs/4 is required, the NCO can be turned off and the coarse modulation block can be used.

This will result in reduced power consumption. The setting for coarse modulation can be found in Register 0x00F, bit 4.

#### **QUADRATURE PHASE CORRECTION**

The purpose of the quadrature phase correction block is to enable compensation of the phase imbalance of the analog quadrature modulator following the DAC. If the quadrature

modulator has a phase imbalance, the unwanted sideband appears with significant energy. Tuning the Quadrature Phase Adjust value can optimize image rejection in single sideband radios.

Ordinarily, the I and Q channels have an angle of precisely 90° between them. The Quadrature Phase Adjustment is used to change the angle between the I and Q channels. When the I Phase Adj[9:0] is set to 1000000000b, the I DAC output moves approximately 1.75° away from the Q DAC output, creating an angle of 91.75° between the channels. When the I Phase Adj[9:0] is set to 0111111111b, the I DAC output moves approximately 1.75° towards the Q DAC output, creating an angle of 88.25° between the channels.

The Q Phase Adj[9:0] works in a similar fashion. When the Q Phase Adj[9:0] is set to 1000000000b, the Q DAC output moves approximately 1.75° away from the I DAC output, creating an angle of 91.75° between the channels. When the Q Phase Adj[9:0] is set to 0111111111b, the Q DAC output moves approximately 1.75° towards the I DAC output, creating an angle of 88.25° between the channels.

Based on these two endpoints, the combined resolution of the phase compensation register is approximately 7°/2048 or 0.00342° per code. The phase adjustment bits can be found in Registers 0x028 and 0x029.

### **DC OFFSET CORRECTION**

The dc value of the I datapath and the Q datapath can be independently controlled by adjusting the I DAC Offset [15:0] and Q DAC Offset [15:0] values in Registers 0x02A thru 0x02B. These values are added directly to the datapath values. Care should be taken not to overrange the transmitted values.



Figure 29. DAC Output Currents vs. DAC Offset Value

Figure 29 shows how the DAC offset current varies as a function of the I DAC Offset [15:0] and Q DAC Offset [15:0] values. With the digital inputs fixed at midscale (0x0000, twos complement data format), the figure shows the nominal  $I<sub>OUTP</sub>$ and I<sub>OUTN</sub> currents as the DAC offset value is swept from 0 to

65535. Because IOUTP and IOUTN are complementary current outputs, the sum of I<sub>OUTP</sub> and I<sub>OUTN</sub> is always 20 mA.

#### **INVERSE SINC FILTER**

The inverse sinc (sinc-1) filter is a 9-tap FIR filter. The composite response of the sinc<sup>-1</sup> and the  $sin(x)/x$  response of the DAC is shown in Figure 30. The composite response has less than  $\pm 0.05$  dB pass-band ripple up to a frequency of  $0.4 \times$ fDACCLK. To provide the necessary peaking at the upper end of the pass band, the inverse sinc filters shown have an intrinsic insertion loss of about 3.2 dB.



Figure 30. Sample composite responses of the sinc<sup>-1</sup> filter with sin(x)/x roll-off



### DAC CLOCK CONFIGURATION

The AD9128 DAC sample clock (DACCLK) can be sourced directly or by clock multiplying. Clock multiplying employs the on-chip Phase Locked Loop (PLL) that accepts a reference clock operating at a sub-multiple of the desired DACCLK rate, most commonly the data input frequency. The PLL then multiplies the reference clock (REFCLK, provided through REFCLKP/N pins) up to the desired DACCLK frequency, which can then be used to generate all the internal clocks required by the DAC. The clock multiplier provides a high quality clock that meets the performance requirements of most applications. Using the on-chip clock multiplier removes the burden of generating and distributing the high speed DACCLK.

The second mode bypasses the clock multiplier circuitry and allows DACCLK to be sourced directly to the DAC core. This mode enables the user to source a very high quality clock directly to the DAC core. Sourcing the DACCLK directly through the DACCLKP, and DACCLKN pins may be necessary in demanding applications that require the lowest possible DAC output noise, particularly when directly synthesizing signals above 150 MHz.

Note that the AD9128 also requires a Frame clock (JESD\_FRAMEP/N) that is used as the master clock for the serial interface. The REFCLK and DACCLK pins are dual-use pins: when not in use, they can be used for DAC alignment (DACALIGNP/N).

### **DRIVING THE DACCLK, REFCLK AND FRAME INPUTS**

The REFCLK and DACCLK differential inputs share similar clock receiver input circuitry. Figure 31 shows a simplified circuit diagram of the input. The on-chip clock receiver has a differential input impedance of about 10 kΩ. It is self biased to a common-mode voltage of about 1.25 V (LVDS compliant). The inputs can be driven by direct coupling differential PECL or LVDS drivers. The inputs can also be ac-coupled if the driving source cannot meet the input compliance voltage of the receiver.



Figure 31. Clock Receiver input equivalent circuit.

If either REFCLKP/N or DACCLKP/N is used for the DACALIGN function, an external 100ohm resistor must be supplied between the two pins (DACALIGNP/DACALIGNN). The minimum input drive level to either of the clock inputs is 200 mV p-p differential. The optimal performance is achieved when the clock input signal is between 800 mV p-p differential and 1.6 V p-p differential. Whether using the on-chip clock multiplier or sourcing the DACCLK, directly, it is necessary that the input clock signal to the device has low jitter and fast edge rates to optimize the DAC noise performance.

#### **DIRECT CLOCKING**

Direct clocking with a low noise clock produces the lowest noise spectral density at the DAC outputs. To select the differential CLK inputs as the source for the DAC sampling clock, set the PLL enable bit (Register 0x018, Bit[7]) to 0. This powers down the internal PLL clock multiplier and selects the input from the DACCLKP and DACCLKN pins as the source for the internal DAC sample clock.

The device also has duty-cycle correction circuitry and differential input level correction circuitry. Enabling these circuits can provide improved performance in some cases. The control bits for these functions can be found in Register 0x019.

### **CLOCK MULTIPLICATION**

The on-chip PLL clock multiplier circuit can be used to generate the DAC sample rate clock from a lower frequency reference clock. When the PLL enable bit (Register 0x018, Bit[7]) is set to 1, the clock multiplication circuit generates the DAC sample clock from the lower rate REFCLK input. The functional diagram of the clock multiplier is shown in Figure 32. The PLL can be setup and controlled through registers 0x018, 0x01A, and 0x01B.

The clock multiplication circuit operates such that the VCO outputs a frequency, fvco, equal to the REFCLK input signal frequency multiplied by  $N1 \times N0$ .

 $f_{VCO} = f_{REFCLK} \times (N1 \times N0)$ 

The DAC sample clock frequency, fDACCLK, is equal to

#### $f_{DACCLK} = f_{REFCLK} \times N1$

The output frequency of the VCO must be chosen to keep f<sub>VCO</sub> in the optimal operating range of 1.0 GHz to 2.1 GHz. The frequency of the reference clock and the values of N1 and N0 must be chosen so that the desired DACCLK frequency can be synthesized and the VCO output frequency is in the correct range.



Figure 32. PLL Clock Multiplication Circuit

#### **PLL SETTINGS**

There are three settings for the PLL circuitry that should be programmed to their nominal values. The PLL values shown in **Table 16** are the recommended settings for these parameters.





#### **CONFIGURING THE VCO TUNING BAND**

The PLL VCO has a valid operating range from approximately 1.0 GHz to 2.1 GHz covered in 63 overlapping frequency bands. For any desired VCO output frequency, there may be several valid PLL band select values. The frequency bands of a typical device are shown in **Error! Reference source not found.**. Device-to-device variations and operating temperature will affect the actual band frequency range. Therefore, it is required that the optimal PLL band select value be determined for each individual device.

#### **Automatic VCO Band Select**

The device has an automatic VCO band select feature on chip. Using the automatic VCO band select feature is a simple and reliable method of configuring the VCO frequency band. This feature is enabled by starting the PLL in manual mode, then placing the PLL in auto band select mode. This is done by setting Register 0x018 to a value of 0xCF, then to a value of

0xA0. When these values are written, the device executes an automated routine that determines the optimal VCO band setting for the device. The setting selected by the device ensures that the PLL remains locked over the full −40°C to +85°C operating temperature range of the device without further adjustment. (The PLL remains locked over the full temperature range even if the temperature during initialization is at one of the temperature extremes.)

## ANALOG OUTPUTS

### **TRANSMIT DAC OPERATION**

 A simplified block diagram of the transmit path DACs is shown in Figure 33. The DAC core consists of a Current Source array, Switch Core, digital control logic, and full-scale output current control. The DAC full-scale output current (IouTFS) is nominally 20 mA. The output currents from the OUTP and OUTN pins are complementary, meaning that the sum of the two currents always equals the full-scale current of the DAC. The digital input code to the DAC determines the effective differential current delivered to the load.





The DAC has a 1.2V bandgap reference with an output impedance of 5 KΩ. The reference output voltage appears on the VREF pin. When using the internal reference, the VREF pin should be decoupled to AVSS with a 0.1µF capacitor. The internal reference should only be used for external circuits that draw DC currents of 2μA or less. For dynamic loads or static loads greater than 2μA, the VREF pin should be buffered. If desired, an external reference (between 1.10V and 1.30V) can be applied to the VREF pin. The internal reference can either be overdriven, or powered down by setting register 0x001 bit 5.



*Figure 34. DAC Full-Scale Current vs. DAC Gain Code* 

For nominal values of VREF (1.2V), RSET (10 k $\Omega$ ), and DAC Gain (512), the full-scale current of the DAC will be typically be 20.16 mA. The DAC full-scale current can be adjusted from

8.66mA to 31.66mA by setting the DAC Gain parameter setting as shown in *Figure 34*.

A 10 kΩ external resistor,  $R_{SET}$ , must be connected from the BIAS RES pin to AVSS. This resistor, along with the reference control amplifier, sets up the correct internal bias currents for the DAC. Because the full-scale current is inversely proportional to this resistor, the tolerance of RSET will be reflected in the full-scale output amplitude.

The equation for the full-scale current is shown below, where DAC gain is set individually for the I and Q DACs in registers 0x02D and 0x003, bit 0 respectively.

$$
I_{FS} = \frac{V_{REF}}{R_{SET}} \times \left(72 + \left(\frac{3}{16} \times DAC \ gain\right)\right)
$$

#### **Transmit DAC Transfer Function**

The output currents from the IOUT1P/2P and IOUT1N/2N pins are complementary, meaning that the sum of the two currents always equals the full-scale current of the DAC. The digital input code to the DAC determines the effective differential current delivered to the load. IOUT1P/2P provides maximum output current when all bits are high. The output currents versus DACCODE for the DAC outputs are expressed as:

$$
I_{\text{OUTP}} = \left[\frac{\text{DACCODE}}{2^N}\right] \times I_{\text{OUTFS}} \tag{1}
$$

$$
I_{OUTN} = I_{OUTFS} - I_{OUTP}
$$
 (2)

where  $DACCODE = 0$  to  $2^N - 1$ .

#### **Transmit DAC Output Configurations**

The optimum noise and distortion performance of the AD9128 is realized when it is configured for differential operation. The common-mode error sources of the DAC outputs are significantly reduced by the common-mode rejection of a transformer or differential amplifier. These common-mode error sources include even-order distortion products and noise. The enhancement in distortion performance becomes more significant as the frequency content of the reconstructed waveform increases and/or its amplitude increases. This is due to the first order cancellation of various dynamic commonmode distortion mechanisms, digital feed-through, and noise.

Figure 35 shows the most basic DAC output circuitry. A pair of resistors, R<sub>O</sub>, is used to convert each of the complementary output currents to a differential voltage output, Vout. Because the current outputs of the DAC are high impedance, the differential driving point impedance of the DAC outputs,  $R_{\text{OUT}}$ , is equal to  $2 \times R_{\text{O}}$ . Figure 36 illustrates the output voltage waveforms.



Figure 35. Basic Transmit DAC Output Circuit



Figure 36. Voltage Output Waveforms

The common-mode signal voltage,  $V_{CM}$ , is calculated as;

$$
V_{CM} = \frac{I_{FS}}{2} \times R_O
$$

The peak output voltage,  $V_{\text{PEAK}}$ , is calculated as

#### $V_{PEAK} = I_{FS} \times R_O$

With this circuit configuration, the single-ended peak voltage is the same as the peak differential output voltage.

#### **Transmit DAC Linear Output Signal Swing**

To achieve optimum performance, the DAC outputs have a linear output compliance voltage range that must be adhered to. The linear output signal swing is dependent on the full-scale output current, I<sub>OUTFS</sub>, and the common-mode level of the output. **Error! Reference source not found.** and **Error! Reference source not found.** show the IMD performance vs. the common-mode voltage at the different full-scale currents and output frequencies.

### APPLICATIONS CIRCUITS

#### **Interfacing to Modulators**

The AD9128 interfaces to the ADL537x family of modulators with a minimal number of components. An example of the recommended interface circuitry is shown in Figure 37.

The baseband inputs of the ADL537x family require a dc bias of 500 mV. The nominal midscale output current on each output of the DAC is 10 mA (½ the full-scale current). Therefore, a single 50  $\Omega$  resistor to ground from each of the DAC outputs results in the desired 500 mV dc common-mode bias for the inputs to the ADL537x. The signal level can be reduced through the addition of the load resistor in parallel with the modulator inputs. The peak-to-peak voltage swing of the transmitted signal is



Figure 37. Typical Interface Circuitry Between the AD9128 and the ADL537x Family of Modulators

#### **BASEBAND FILTER IMPLEMENTATION**

Many applications require a baseband anti-imaging filter between the DAC and the modulator to filter out Nyquist images and broadband DAC noise. The filter can be inserted between the I-V resistors at the DAC output and the signal-level setting resistor across the modulator input. Doing this establishes the input and output impedances for the filter.

Figure 39 shows a fifth-order, low-pass filter. A common-mode choke is used between the I-V resistors and the remainder of the filter. This removes the common-mode signal produced by the DAC and prevents the common-mode signal from being converted to a differential signal, which can appear as unwanted spurious signals in the output spectrum. Splitting the first filter capacitor into two and grounding the center point creates a common-mode low-pass filter, providing additional commonmode rejection of high frequency signals. A purely differential filter can pass common-mode signals.

#### **DRIVING THE ADL5375-15**

The ADL5375-15 requires a 1500 mV dc bias and, therefore, requires a slightly more complex interface than most other Analog Devices, Inc, modulators. It is necessary to level shift the DAC output from a 500 mV dc bias to the 1500 mV dc bias that the ADL5375-15 requires. Level shifting can be achieved with a purely passive network, as shown in Figure 38. In this +network, the dc bias of the DAC remains at 500 mV while the input to the ADL5375-15 is 1500 mV. This passive, level shifting network introduces approximately 2 dB of loss in the ac signal.



Figure 38. Passive, Level Shifting Network for Biasing ADL5375-15

#### **REDUCING LO LEAKAGE AND UNWANTED SIDEBANDS**

Analog quadrature modulators can introduce unwanted signals at the LO frequency due to dc offset voltages in the I and Q baseband inputs, as well as feedthrough paths from the LO input to the output. The LO feedthrough can be nulled by applying the correct dc offset voltages at the DAC output. This can be done using the by using the digital DC offset adjustments (Registers 0x02A and 0x02B).

Good sideband suppression requires both gain and phase matching of the I and Q signals. The I/Q phase adjust (Register 0x028 amd 0x029) and DAC FS adjust (Register 0x02D and Register 0x02F) registers can be used to calibrate I and Q transmit paths to optimize the sideband suppression.



Figure 39. DAC Modulator Interface with Fifth-Order, Low Pass Filter

### **SERDES LINK PRINTED CIRCUIT BOARD DESIGN CONSIDERATIONS**

### MULTI-CHIP ALIGNMENT AND LATENCY LOCK

**Note:** If an internal frame clock signal is used, it is recommended that this configuration be setup prior to the configuration of the SERDES PLL.

This feature of the AD9128 enables multiple Dual DACs to be synchronized with each other. It also ensures a constant latency for each of the Dual DACs: in addition to all the DACs being synchronized, the latency of each DAC in the multi-chip system will be constant from link establishment to link establishment. In order to achieve this, the AD9128:

- Makes provision for an external alignment signal (DACALIGN) to be supplied to all the DACs
- Allows for the SYNCb launch timing of each of the DACs to be individually controlled. The SYNCb signal can be delayed by integral multiples of the frame clock signal. It can also be finely tuned using the SYNCb DLL. The SYNCb interface and usage models are described in detail later in this section.

### **EXTERNAL ALIGNMENT SIGNAL**

In order to align multiple DACs to one another, an external differential DACALIGN edge may be required (see **SYNCb usage models** section). The alignment operation is done on a single edge of the differential DACALIGNP/N input. Note that DACALIGNP/N should be fed to the appropriate pins:

- a. If DACCLKP/N is being used as the clock: DACALIGNP/N must be fed to the REFCLKP/N pins.
- b. If the internal DAC PLL is being used to generate the clock: DACALIGNP/N must be fed to the DACCLKP/N pins.

In both cases, if DACALIGN is used, AC coupling cannot be employed. It should be an LVDS signal and a 100 ohm termination resistor should be placed between the pins used as DACALIGNP/N.

The external DACALIGN edge in conjunction with other internal clocks will be used to reset the interpolation clocks and the multi-frame counter of the DAC. The DACALIGN modes are controlled through register 0x00C. Bit 7 enables the use of the DACALIGN edge for DAC alignment. There are three possible scenarios in this case:

• The DACs can be aligned with the Frame clock. In this case, bit 5 of register 0x00C must be set. If set, the DACALIGN edge will be sampled by the next frame clock edge. The following rising edge of that frame clock will be sampled by the DAC clock and used as the alignment edge for the DAC reset.

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In order to ensure accurate alignment, a keep out window will exist between the DAC clock and the input Frame clock reference. This is required such that the same DAC clock samples the frame pulse on all DACs. A keep-out window will also exist between the Frame clock and the DACALIGN edge in order that the same Frame clock period is used by all DACs as a sampled alignment signal. (Keep-out specification TBD).

- The DACs can be aligned directly to the DACALIGN signal. In this case, bit 5 should not be set.
- In systems where external DACALIGN signal is not used, but the user would still like to align the DAC interpolation clocks to the reference/frame clock, bit 2 of register 0x00C must be set. In order for this mode to work, bit 5 of register 0x00C must be set high prior to setting bit 2. As with option 1, a keep out window will exist between the DAC clock and the input Frame clock reference.

#### **SYNCB INTERFACE**

The SYNCb interface is used to establish and communicate code group synchronization between the JESD204A deframer block and the transmitter (in accordance with the JESD204A specifications). The interface can be setup and monitored through registers 0x00A and 0x00B.

In order to enable multi-chip synchronization, the launch timing of the SYNCb signal can be either finely or coarsely controlled. If the user requires fine timing control of the SYNCb interface, the SYNCb DLL can be enabled through register 0x00B bit 7. The DLL locks on to the frame clock of the system (register 0x00B bit 6 can be read to check if the DLL has successfully locked). Note that if the internal DAC PLL is being used for the DAC clock, then the DLL should be enabled after a lock on the DAC PLL has been achieved (see section *DAC Clock Configuration* for details on DAC PLL).

The SYNCb delay offset can be manually set through register 0x00B bits 4:2 (see *User Algorithm* section below) or autocalibrated by setting register 0x00A bit 4 high (see *Automated Algorithm* below).

#### **User Algorithm**

 While the periodic SYNCb signal is being emitted, the FPGA can sweep the values to the SYNCB phase selector register (Reg 0x00B bit1:0 can be used to generate a periodic signal on SYNCb).

• The FPGA should be able to count the number of high and low captures on the periodic waveform with its FRAME clock. For instance, if register 0x00B bits1:0 are set to 11, there will be 4 high captures followed by 4 low captures.

- Consequently, the FPGA counter should expect 4 high and 4 low captures. When the SYNCb phase selection is changed and the FPGA counter deviates from a count of 4 (either 3 or 5 for one period f SYNCb oscillation), it implies that the SYNCb edge has passed over a FPGA frame clock boundary.
- The algorithm can then select a DLL phase 4 phases away from the phase producing the deviation. It is recommended that the DLL phase is the center of the capture eye.
- Also note that if the phase chosen is greater than the phase producing the deviation, then the user should apply a value of 1 to the Additional Latency Register (0x015). This is necessary in order to compensate for the extra delay in the chain produced by the SYNCb handoff to the FPGA.

#### **Automated Algorithm**

The AD9128 can also attempt to automatically find the center of the sampling eye. This can be done by setting bits 6 and 4 of register 0x00A. Note that the AD9128 must be programmed appropriately so that the data link can be successfully enabled.

- The automated algorithm will enable the link and capture the round trip delay from SYNCb to the datapath input of the DAC and record it.
- It will then sweep the phase selection for SYNCb launch backwards until the round trip delay changes. This is recorded as the first frame clock boundary of the FPGA.
- It will reset the phase selection to zero, calculate the round trip and sweep the phase selection forward until the round trip changes. This is recorded as the second frame clock boundary.
- It will then choose a phase halfway between the two edges, and record that value as the selected SYNCb phase. This phase will be readable through the register 0x00B bits 4:2 as long as bit 4 of Register 0x00A remains set.

#### **SYNCB USAGE MODELS**

The SYNCb setup for multi-chip synchronization can be handled in 2 ways:

#### **SPI interface**

This option is possible only when the DACs establish their own individual link with a common external frame clock (SYNCb signals are not combined at the transmitter). This scenario is depicted in Figure 38.If each DAC exists on its own JESD204A link within the system, there exists no path for communication between the DACs since the SYNCb signals are sent individually to the transmitter. If one lane loses lock, only that transmit link is compromised. SPI based synchronization is sufficient and can be accomplished through setting bits 2 and 5

of register 0x00C (bit 4 optional). The Align to frame request (Register 0x00C, bit 2) will allow the internal SYNCb FIFO reset to be determinant and guarantees the same forward path latency on each of the independent links.

#### **External alignment signal (DACALIGN) a. If user supplies external frame clock:**

If the SYNCb signals from the DACs are combined at the transmitter, then an external alignment (DACALIGN) signal is needed for all the DACs. Bits 5 and 7 of register 0x00C must be set high (bits 6 and 4 optional) in this case bit 2. This will ensure that the multi-chip alignment is based on the frame source clock. This scenario is depicted in Figure 41.



**NOTE 1: EITHER EXTERNAL OR INTERNAL FRAME CLOCK CAN BE USED**

Figure 40.Multichip operation when each DAC operates with an independent autonomous link



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Figure 41. Mult-chip synchronization with external DACALIGN signal when SYNCb is combined at the transmitter

#### **b. If internal frame clock is used:**

If user supplies DAC clock only and no frame clock (frame clock generated internally in the DAC), then DACALIGN signal must be applied to all the DACs with Register 0x00C set to 0xD0. The internal frame clock should also be locked to the internal data rate clock (Register 0x01D set to 0x30). Note that calibration of the SYNCb interface must be performed after the DACALIGN signal is applied.

In addition to setting the modes of operation for the Multichip alignment, the value of the transmitter's latency should be written into register 0x014 bits 4:0. This latency is measured in frame clock periods through the transmitter from SYNCb capture to the time when the first ILAS symbol leaves the transmitter. This value, typically a fractional number of frame clock periods, should be rounded to the nearest whole number

of frame clock cycles. If the TX latency is not known, a diagnostic mode can be used to find this value:

- Set Register 0x013 bit 5 high for each DAC in the system
- The additional latency to be used is generated in Register 0x015 bits 4:0 after the link is established.
- The average additional latency (for all DACs) generated by this mode should be used as the common TX latency for all DACs

When (re)alignment is required, DACALIGN signal must be transitioned to its pre-alignment value (default: low) and set (default: high) again. Using the above methods for multi-chip alignment will ensure that the latency of the forward path will remain constant from link establishment to link establishment. The only exception could occur if the DAC experiences a power glitch.

### AD9128 STARTUP SEQUENCE AND LATENCY ALIGNMENT PROCEDURE

This section describes the recommended start-up sequence for the AD9128. And presents two alternative sequences for performing deterministic latency alignment among two or more AD9128 devices.

### **STARTUP FLOWCHART**



Figure 42. Start-up sequence Flow Chart for the AD9128

### **MULTI-CHIP LATENCY ALIGNMENT FLOWCHART**



Figure 43. . Multi-Chip Latency Alignment Flow Chart for the AD9128







Figure 44. Latency Alignment Scheme A

In latency alignment scheme A, the DACALIGN signal from the JESD204 transmitter tells each AD9128 which edge of the DAC sampling clock to use to reset it's LMFC (local multiframe counter).





FPGA or ASIC Containing JESD204 Transmitter

Figure 45. Latency Alignment Scheme B

In latency alignment scheme B, the DACLIGN signal from the JESD204 transmitter tells each AD9128 which edge of FRAME\_P/FRAME\_N to use to reset each AD9128's LMFC.

#### Transmitter Setup for AD9128 Latency Alignment





Figure 46. DACALIGN Transmitter Output and Transmitter LMFC Timing



D1 = Delay from LMFC rising edge to ILAS start at Tx Framer output

D2 = Delay from Transmitter Framer output to Transmitter Output D3 = Delay from Receiver Input to Internal Shift Register (Receiver Latency),  $D3 = 34$  in AD9128

The unit of Delay is Samples. In HuaWei's system 1 Frame = 1 Sample = 1 Byte

Calculations:  $X = D1 + D2 + D3 = D1 + D2 + 34$  $Y = X$  MOD 32  $D4 = 32 - Y$ 

ILAS: Inter-Lane Alignment Sequence LMFC: Local Multi-Frame Clock

Figure 47. Calculating the D4 Delay Time

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### TESTING THE SERDES LINK AT THE BOARD LEVEL

### REGISTER MAP



<sup>1</sup> Align Machine (0x0C[3]) must be enabled before writing to this register.





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### REGISTER DESCRIPTIONS

**WARNING: Unspecified registers are unused/reserved and should not be written to. Reading from unused register may give unexpected results.** 





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<sup>1</sup> All bits are high when interrupt is active. Clear interrupt by writing respective service bit HIGH. Reading these bits when interrupt enable is not set reads back the instantaneous value of the triggering event



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configuration



only

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**for the given lane address.**



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### **Note: The write values for this register are described above. The read value for this register is the NIT error count for the given lane address**



### **Note: The write values for this register are described above. The read value for this register is the Unexpected K- character error count for the given lane address.**









### OUTLINE DIMENSIONS





#### **ORDERING GUIDE**



